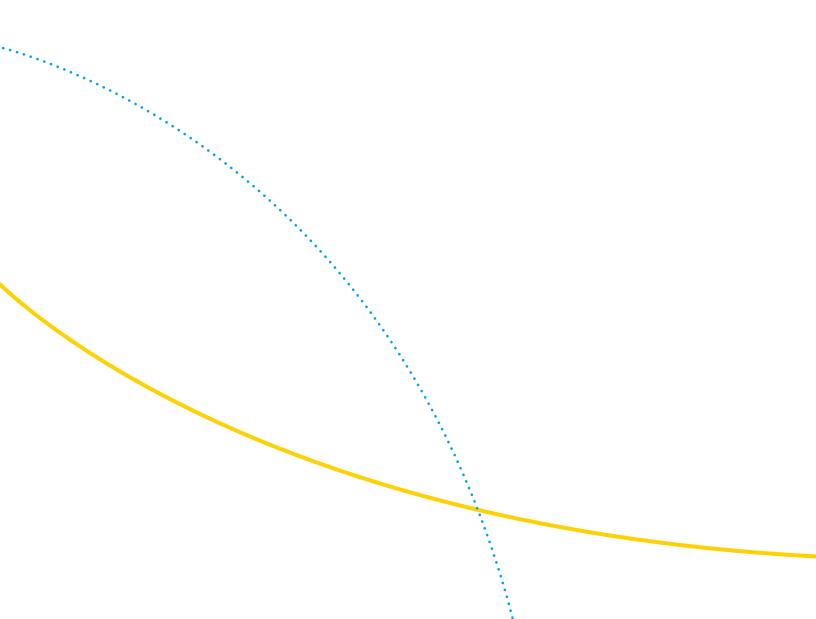


# Testing and Analysis of Surface Mounted Lead Free Soldering Materials and Processes

Presented at IPC SMEMA Council APEX® 2003



### **Abstract**

The Massachusetts Toxics Use Reduction Institute (TURI) has sponsored a consortium of Massachusetts based corporations to investigate leadfree (Pb-free) surface mount soldering technology. The current effort is a Design of Experiments (DOE) analysis using three NEMI recommended tin silver copper (SnAgCu) alloys from three different solder manufacturers, five Ph-free PWB surface finishes, and two reflow environments. The consortium designed a special test PWB and that was used in the experiments. A modified visual test procedure was developed and the results are presented based on statistical analysis. Test PWBs with BGAs, leaded and chip components will be subjected to thermal cycling, and then tested for mechanical degradation. Standard tin-lead (SnPb) eutectic solder 63/37 reflow samples were used as a control.

Components on these test substrates include plastic and ceramic leaded SOICs, FPQFPs, an LCC, 45mm square ball grid arrays (BGAs) and small passive devices. This paper will discuss results along with the issues associated with each lead and PWB finish. Conclusions from this paper can be used as a guide to future product offerings, and to proper testing, reporting methods and recommendations to satisfy future Pb-free requirements.

### Introduction

Currently, a large number of "toxic" materials used in electronics manufacture are under scrutiny. Legislation is in place or being considered to restrict, limit, or outright ban the use of Pb (lead) and brominated polymer flame-retardants used in electronics as well as other materials. Japan has implemented Pb-Free Electronics Guidelines and the European Economic Union is considering takeback and removal (WEEE-Waste Electrical and Electronic Equipment)[1] or outright banning import (RoHS-Restriction of Hazardous Substances) [2] while the US EPA is working on TRI (Toxics Release Inventory)[3] reporting of hazardous components.

Massachusetts has founded the Toxics Use Reduction Institute (TURI) to assist companies in reducing their use of toxic substances. They have funded a number of university led programs including Pb-free electronics assembly development. To increase the scope of this effort, the University of Massachusetts—Lowell, has formed a consortium of local industries to help develop Pb-free electronics. Corporate members are: Air Products and Chemicals, Analog Devices, BTU International, M/A-COM, Raytheon, Sanmina-SCI. Schneider Electric-Automation Business, and Texas Instruments.

Several studies (DOEs) have already been published. [4-7] The effort this year is focusing on solder composition, PWB finishes (solderability preservatives), and lead finishes.

## Experimental Design Matrix

A designed experiment was developed with the following variables:

- 1. **PWB Finishes**—Five Treatments—
  Solder Mask Over Bare Copper with
  Hot Air Solder Leveling (SMOBC/
  HASL), Matte Finish Tin (Sn)
  Electroplate, Immersion Silver (Ag),
  Organic Solder Preservative (OSP),
  and Electroless Nickel Immersion
  Gold (ENIG).
- 2. **Reflow Atmospheres**—Two Treatments—Air and Nitrogen.
- 3. **Solder Pastes**—Three Treatments—all with the same alloy composition—95.5Sn-3.8 Ag-0.7Cu (NEMI recommended) from three different vendors, all incorporating no-clean fluxes.
- 4. **Component Lead Finishes**—Four Treatments—matte Sn plating, Tin/Silver/Copper, Nickel/Palladium/Gold, and Nickel/Gold.
- Sn-Pb eutectic solder PWB using the solder treatments as control PWBs.

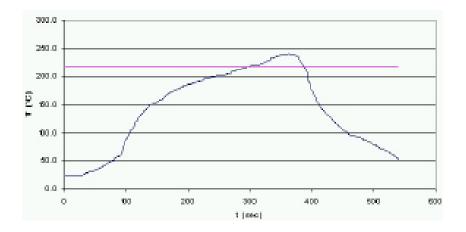
The Design matrix is shown in Table 1.

Table 1: Experimental Design Matrix (Two (2) Circuit Boards per Trial)

| PWB | PWB Finish | Solder paste   | Reflow Atmosphere* | Component Finish |
|-----|------------|----------------|--------------------|------------------|
| 1   | SMOBC/HASL | "A"            | Air                | Pb- free         |
| 2   | SMOBC/HASL | "A"            | Nitrogen           | Pb- free         |
| 3   | SMOBC/HASL | "B"            | Air                | Pb- free         |
| 4   | SMOBC/HASL | "B"            | Nitrogen           | Pb- free         |
| 5   | SMOBC/HASL | "C"            | Air                | Pb- free         |
| 6   | SMOBC/HASL | "C"            | Nitrogen           | Pb- free         |
| 7   | SMOBC/HASL | Standard Sn-Pb | Air                | Sn-Pb Leads      |
| 8   | OSP        | "A"            | Air                | Pb- free         |
| 9   | OSP        | "A"            | Nitrogen           | Pb- free         |
| 10  | OSP        | "B"            | Air                | Pb- free         |
| 11  | OSP        | "B"            | Nitrogen           | Pb- free         |
| 12  | OSP        | "C"            | Air                | Pb- free         |
| 13  | OSP        | "C"            | Nitrogen           | Pb- free         |
| 14  | OSP        | Standard Sn-Pb | Air                | Sn-Pb Leads      |
| 15  | ENIG       | "A"            | Air                | Pb- free         |
| 16  | ENIG       | "A"            | Nitrogen           | Pb- free         |
| 17  | ENIG       | "B"            | Air                | Pb- free         |
| 18  | ENIG       | "B"            | Nitrogen           | Pb- free         |
| 19  | ENIG       | "C"            | Air                | Pb- free         |
| 20  | ENIG       | "C"            | Nitrogen           | Pb- free         |
| 21  | ENIG       | Standard Sn-Pb | Air                | Sn-Pb Leads      |
| 22  | Matte Sn   | "A"            | Air                | Pb- free         |
| 23  | Matte Sn   | "A"            | Nitrogen           | Pb- free         |
| 24  | Matte Sn   | "B"            | Air                | Pb- free         |
| 25  | Matte Sn   | "B"            | Nitrogen           | Pb- free         |
| 26  | Matte Sn   | "C"            | Air                | Pb- free         |
| 27  | Matte Sn   | "C"            | Nitrogen           | Pb- free         |
| 28  | Matte Sn   | Standard Sn-Pb | Air                | Sn-Pb Leads      |
| 29  | Ag         | "A"            | Air                | Pb- free         |
| 30  | Ag         | "A"            | Nitrogen           | Pb- free         |
| 31  | Ag         | "B"            | Air                | Pb- free         |
| 32  | Ag         | "B"            | Nitrogen           | Pb- free         |
| 33  | Ag         | "C"            | Air                | Pb- free         |
| 34  | Ag         | "C"            | Nitrogen           | Pb- free         |
| 35  | Ag         | Standard Sn-Pb | Air                | Sn-Pb Leads      |

<sup>\*</sup>Nitrogen was supplied by Air Products and Chemicals, Inc. and contained 50 ppm Oxygen for these experiments.

Figure 1: Reflow Profile for SMT Board Assembly



As seen, all test PWBs were run versus the standard 63Sn-37Pb eutectic, no-clean solder as a control. Package types included several SOICs, a FPQFP, an MLP, a BGA, a ceramic SOIC, and chip capacitors and resistors.

The test PWB was laid out at M/A-COM taking into account daisy chain resistance test capabilities in some of the parts and fabricated by Sanmina-SCI with the five different finishes. Pastes were obtained from three vendors and a reflow profile was developed based on the manufacturers' product data sheets. A reflow profile board was populated with parts and three K-probe thermocouples (TC) were attached to the surface. One TC was attached at the leading edge of the PWB, one at the lead attach area of a large QFP and one near the trailing edge. The thermocouples were connected to an industry standard data logger. The thermal readings were downloaded to the data collector software for comparison to the manufacturer recommended profiles. All three manufacturers recommended a 'ramp to spike' curve. Several runs were performed to ensure consistent performance. The reflow profile used for all three Pb-free solders is shown in Figure 1. Solder paste prints were made using a 0.006" thick stainless steel laser cut, electropolished stencil.

Ten percent aperture reductions were used on the fine pitch devices. PWBs were assembled at Schneider Electric on their assembly line consisting of an MPM AP-25 screen printer, Siemens S20 and F5 placement equipment and a BTU Pyramax 98N Reflow Oven with Air and Nitrogen capability supplied by BTU International for this experiment. The Schneider plant maintains a Relative Humidity (RH) level between 35–40%.

After reflow, boards were packaged in ESD bags and taken to M/A-COM where two University of Massachusetts—Lowell senior students visually inspected the solder joints based on training by a certified IPC inspector/trainer. Inspection criteria were established as follows: total defects, cold solder joints, non-wetting, solder balls, dewetting, bridging, pinholes, shiny appearance, smooth appearance, and flux residue. X-ray radiography of the BGA solder joints was also performed. Initial inspection data has been tabulated and statistically analyzed by University of Massachusetts—Lowell and Air Products. To date board finish, atmosphere, and paste (A, B, C) have been analyzed. See Tables 3, 4, and 5. Work is in progress on lead finish and component type.

### **Results**

### **Assembly Process**

The major difficulties encountered in assembly were with stencil printing and placement system vision. In spite of using print parameters close to those in the application notes supplied for the three pastes, paste A had a tendency to adhere to the sides of the stencil openings. This resulted in scant prints on some of the fine pitch apertures. Paste B clogged the necessitating cleaning after every four or five prints. Paste C performed as expected with little difficulty. All three pastes exhibited good tack or component holding qualities during and after placement. Vision problems were associated with the Sn-Pb version of the BGA. The difference in appearance (reflectivity) of the Sn-Pb spheres caused the vision system (programmed for the Pb-free spheres) to reject many of the Sn-Pb BGAs. These had to be placed by hand which may affect some results.

#### Visual Defects—Statistics

Eight main categories of common defects were selected and all boards were inspected. Those defects observed were photographed and recorded into a spreadsheet. After statistical analysis the following significant effects were determined (all shown by the letter Y and a number indicating the rank starting with 1 being the most significant).

As seen in Table 2, the two major defects observed were cold solder joints and non-wetting. All major variables impacted these two defects and a significant interaction effect between paste and atmosphere on cold solder joints was also observed. Solder ball defects were also impacted by board finish. Some variables also had a significant effect on the solder joint appearance with respect to shininess and flux residue. Since Pb-free solder is different in appearance, these were considered important as well.

**Table 2: Statistically Significant Effects Summary** 

|                     |        |             |            |                  | 2 Factor              |                      | 3 Factor                     |
|---------------------|--------|-------------|------------|------------------|-----------------------|----------------------|------------------------------|
|                     |        | Main Effect | ts         |                  | Interactions          |                      | Interaction                  |
| Property            | Finish | Paste       | Atmosphere | Finish*<br>Paste | Finish*<br>Atmosphere | Paste*<br>Atmosphere | Finish* Paste*<br>Atmosphere |
| Total Defects       | Y - 3  | Y - 2       | Y - 1      | Ν                | N                     | Υ                    | Ν                            |
| Cold Solder Joining | Y - 3  | Y - 2       | Y - 1      | N                | N                     | Υ                    | N                            |
| Nonwetting          | N      | Y - 2       | Y - 1      | N                | N                     | N                    | N                            |
| Solder Balls        | Υ      | N           | Ν          | Ν                | N                     | N                    | N                            |
| Dewetting           | N      | N           | Ν          | Ν                | N                     | N                    | N                            |
| Bridging            | Υ      | N           | Ν          | Ν                | N                     | N                    | N                            |
| Pin/Blow Holes*     | N      | N           | N          | Ν                | N                     | N                    | N                            |
| Shiny**             | Y - 1  | Y - 2       | N          | Ν                | N                     | N                    | N                            |
| Residue**           | N      | Y - 1       | Y - 2      | N                | N                     | N                    | N                            |
| Smooth**            | N      | N           | N          | N                | N                     | N                    | N                            |

Table 3: Atmosphere Results Summary

|                     | Atmo   | sphere   |
|---------------------|--------|----------|
| Property            | Air    | Nitrogen |
| Total Defects       | 150.30 | 6.00     |
| Cold Solder Joining | 102.70 | 1.10     |
| Nonwetting          | 33.30  | 1.60     |
| Solder Balls        | 9.07   | 2.83     |
| Dewetting           | 5.10   | 0.43     |
| Bridging            | 0.13   | 0.03     |
| Pin/Blow Holes*     | 0.00   | 0.00     |
| Shiny**             | 0.63   | 0.43     |
| Residue**           | 0.83   | 0.47     |
| Smooth**            | 0.80   | 0.97     |

Nitrogen reflow atmosphere was shown to be significant in total defects, cold solder joints, non-wetting and residue generated.

### **Legend for All Tables**

- \* Pin/Blow Holes: No defects of this type were observed
- \*\* Qualitatively measured properties

Statistically significant effects are bolded and in blue.

Table 4: Pb-Free Paste Results Summary

|                     | Pb-Free Paste |        |       |  |  |
|---------------------|---------------|--------|-------|--|--|
| Property            | В             | Α      | С     |  |  |
| Total Defects       | 11.35         | 171.25 | 51.90 |  |  |
| Cold Solder Joining | 0.20          | 137.45 | 18.10 |  |  |
| Nonwetting          | 2.60          | 20.25  | 29.50 |  |  |
| Solder Balls        | 8.00          | 6.35   | 3.50  |  |  |
| Dewetting           | 0.50          | 7.15   | 0.65  |  |  |
| Bridging            | 0.05          | 0.05   | 0.15  |  |  |
| Pin/Blow Holes*     | 0.00          | 0.00   | 0.00  |  |  |
| Shiny**             | 0.80          | 0.30   | 0.50  |  |  |
| Residue**           | 0.85          | 0.70   | 0.40  |  |  |
| Smooth**            | 0.95          | 0.90   | 0.80  |  |  |

A statistically significant Paste effect means that one or more of the pastes studied differ significantly from each other in terms of the type and/or number of defects generated. Significance is noted with bold numbers.

Table 5: Board Surface Finish Results Summary

| Property            | ENIG  | Imm. AG | Finish Matte Sn | OSP    | SMOBC/HASL |
|---------------------|-------|---------|-----------------|--------|------------|
| Total Defects       | 20.42 | 29.67   | 62.92           | 107.58 | 170.25     |
| Cold Solder Joining | 5.83  | 13.83   | 43.75           | 101.75 | 94.42      |
| Nonwetting          | 7.75  | 13.42   | 6.50            | 3.50   | 56.08      |
| Solder Balls        | 6.08  | 2.00    | 1.33            | 1.67   | 18.67      |
| Dewetting           | 0.75  | 0.42    | 11.33           | 0.67   | 0.67       |
| Bridging            | 0.00  | 0.00    | 0.00            | 0.00   | 0.42       |
| Pin/Blow Holes*     | 0.00  | 0.00    | 0.00            | 0.00   | 0.00       |
| Shiny**             | 0.17  | 0.75    | 0.50            | 0.67   | 0.58       |
| Residue**           | 0.83  | 0.58    | 0.42            | 0.67   | 0.75       |
| Smooth**            | 0.83  | 0.92    | 0.75            | 0.92   | 1.00       |
|                     |       |         |                 |        |            |

A statistically significant Board Finish effect means that one or more of the surface finishes studied differ significantly from each other. Significance is noted with bold numbers

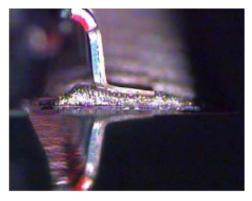
### Visual Defects—Images

Following (Figures 2–10) are some representative photographs of several solder joint visual defects and appearance issues on various package types.

Figure 2:

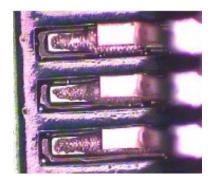


The Expected Higher Wetting Angles for Pb-Free Solder Joints are observed

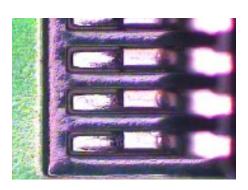


Non-Coalesced Paste Spheres are Seen in this Air Reflow Sample Paste A on SMOBC-HASL

Figure 3:

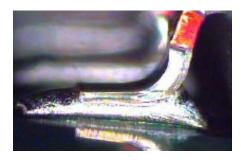


Paste A Reflowed in Air



Paste A in Nitrogen—Fine Pitch Print, Ni-Pd-Au Lead—SMOBC-HASL

Figure 4: Paste A in Air, SOIC Leads on the Same Board

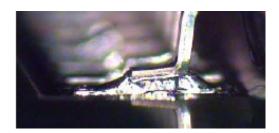


Lead Finish Plated Tin



Ni-Pd-Au Plated Leads—SMOBC-HASL

Figure 5: Paste B in Air

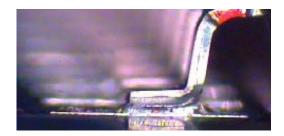


Past B in Nitrogen



SMOBC-HASL

Figure 6: Paste C in Air

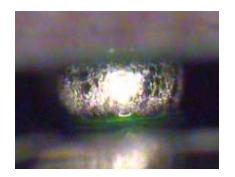


Paste C in Nitrogen

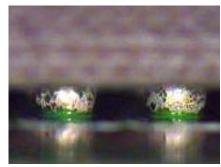


SMOBC-HASL

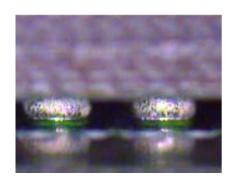
Figure 7: BGA Solder Joints



Paste A in Air—SMOBC-HASL



Paste B in Nitrogen—ENIG

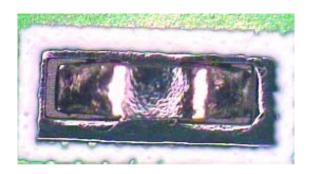


Paste C in Air—ENIG

Figure 8: Pb-Free (Sn) Resistors — Paste C on Immersion Silver



Paste A Reflowed in Air



Paste A in Nitrogen—Fine Pitch Print, Ni-Pd-Au Lead—SMOBC-HASL

Figure 9: Paste B in Nitrogen on SMOBC-HASL—Gold Lead Finish

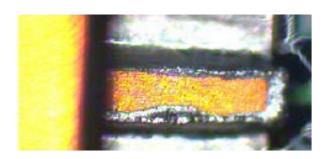
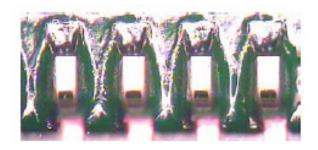


Figure 10: Pb-Sn reflow control—Sn Leads on Matte Tin Finish



Other experimental results to be reported later include: 1) BGA sphere attach experiments, 2) x-ray analysis for voids and BGA bridging, 3) oxygen content of reflow Nitrogen effects, 4) effects of reflow profile, 5) and pull and shear test data before and after thermal cycling.

### **Discussion**

Visual inspection, of course, does not tell the entire story. It is a good method of finding many defects but does not reveal weak solder joints, large internal voids, or many BGA solder joint defects. Moreover, the correlation between appearance and reliability has not been established for Pb-free solders, in the way that it has for Sn63type solders. This correlation will be explored during the continuation of this study. Based on Figure 11, ENIG, Paste "B," and Nitrogen would be considered "winners" with Ag a close second for board finish. Within the confines of effect of these variables on visual defects/appearance issues this is correct. However, manufacturing cost issues were not addressed as part of the overall analysis. Nitrogen does cost more than using ambient air so defect costs may have to be offset by Nitrogen costs. Electroless nickel used in ENIG has often been associated with "black pad" solderability defects (not an issue in this study) that may occur in some circuit card assemblies. As noted above, Paste B clogged the stencil requiring cleaning after every four or five prints and thus could have a large effect on throughput and other line costs.

Consider Figure 3. Paste A clung to the aperture walls during printing resulting in scant prints on fine pitch pads. The flux tended to flow during reflow ramp and soak and so, with an inappropriate volume of paste, was not able to prevent the paste spheres from re-oxidizing before reflow. The paste under the lead did wet and flow, as did areas with more paste volume. Perhaps an experiment to develop a better stencil print would improve this result. The other alternative, Nitrogen, is more forgiving so this paste may be fine for larger pitch or when using Nitrogen for a reflow atmosphere.

Returning to Figure 11, Paste "C" had more defects, mainly in Air, but also gave a good print nearly every board. Experiments may improve performance for all pastes, "C," "B," and "A". One must also consider that these pastes are not necessarily fully developed with good histories as Pb-free processing itself is still in its infancy.

Figures 4—8 all show solder joints with "acceptable" appearances if one considers the higher wetting angle associated with Pb-free pastes. Figure 9 shows the effect of a thick gold finish on reflow. The results are similar to what one would find in a eutectic Sn-Pb solder joint. The gold, as it dissolves in the molten solder, raises the melting temperature in the limited solder volume available to the point when further wetting is "frozen out" leaving a wave front as shown.

Figure 11: Defect Density Versus Independent Variables

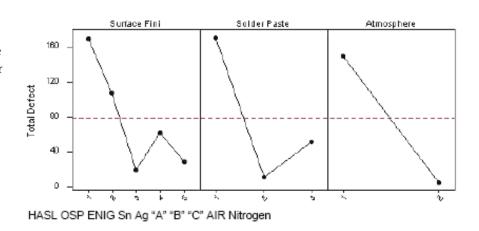


Table 6: Statistical Analysis — Total Defects

|                         | ANOVA    | for 0.35 Power Transfor | med Total Defect Data |          |        |  |  |
|-------------------------|----------|-------------------------|-----------------------|----------|--------|--|--|
| The GLM Procedure       |          |                         |                       |          |        |  |  |
|                         |          | Dependent Variable:     | Total Defect          |          |        |  |  |
| Source                  | DF       | Sum of Squares          | Mean Square           | F Value  | Pr > F |  |  |
| Model                   | 29       | 363.4838458             | 12.5339257            | 8.23     | <.0001 |  |  |
| Error                   | 30       | 45.7076735              | 1.5235891             |          |        |  |  |
| Corrected Total         | 59       | 409.1915194             |                       |          |        |  |  |
|                         | D. C     | Cooff)/or               | D+ MCF                | TD M     |        |  |  |
|                         | R-Square | Coeff Var               | Root MSE              | TD Mean  |        |  |  |
|                         | 0.888298 | 43.38638                | 1.234338              | 2.844989 |        |  |  |
| Source                  | DF       | Type III SS             | Mean Square           | F Value  | Pr > F |  |  |
| Board Finish            | 4        | 44.6816022              | 11.1704005            | 7.33     | 0.0003 |  |  |
| Paste                   | 2        | 78.9621665              | 39.4810833            | 25.91    | <.0001 |  |  |
| Atmosphere              | 1        | 132.3624551             | 132.3624551           | 86.88    | <.0001 |  |  |
| Finish*Paste            | 8        | 16.0395976              | 2.0049497             | 1.32     | 0.2735 |  |  |
| Finish*Atmosphere       | 4        | 15.2827444              | 3.8206861             | 2.51     | 0.0629 |  |  |
| Paste*Atmosphere        | 2        | 54.3289039              | 27.1644519            | 17.83    | <.0001 |  |  |
| Finish*Paste*Atmosphere | 8        | 21.8263762              | 2.7282970             | 1.79     | 0.1184 |  |  |

As seen above, the ANOVA (Analysis of Variance) is significant for the overall experiment and for the variables highlighted with probabilities Pr less than .05.

| Ryan-Einot-Gabriel-Welsch Multiple Range Test for Total Defects (Board Finish)    |        |    |            |  |  |  |  |
|---|--------|----|------------|--|--|--|--|
| Means with the same REGWQ Grouping letter (A, B) are not significantly different. |        |    |            |  |  |  |  |
| REGWQ Grouping  | Mean   | N  | Finish     |  |  |  |  |
| А   | 170.25 | 12 | SMOBC/HASL |  |  |  |  |
| В   | 107.58 | 12 | OSP        |  |  |  |  |
| В   | 62.92  | 12 | Matte Sn   |  |  |  |  |
| В   | 29.67  | 12 | Imm. AG    |  |  |  |  |
| В   | 20.42  | 12 | ENIG       |  |  |  |  |

**Interpretation:** The Board Finish level SMOBC/HASL significantly differs from all other finishes. No other finishes were found to be statistically different from one another at the 0.05 level.

| Ryan-Einot-Gabriel-Welsch Multiple Range Test for Total Defects (Paste)  Means with the same REGWQ Grouping letter (A, B,) are not significantly different. |           |   |         |  |  |
|---|-----------|---|---------|--|--|
| REGWQ Grouping  | Mean      | N | Finish  |  |  |
| А   | 171.25 20 | А | Pb-Free |  |  |
| В   | 51.90 20  | С | Pb      |  |  |
| С   | 11.35 20  | В | Pb      |  |  |

**Interpretation:** All Pastes were found to differ significantly from all other pastes. B Pb-Free performed best.

| Ryan-Einot-Gabriel-Welsch Multiple Range Test for Total Defects (Atmosphere)  Means with the same REGWQ Grouping letter (A, B,) are not significantly different. |        |    |            |  |  |  |
|--|--------|----|------------|--|--|--|
| REGWQ Grouping   | Mean   | N  | Atmosphere |  |  |  |
| А  | 150.33 | 30 | Air        |  |  |  |
| В  | 6.00   | 30 | Nitrogen   |  |  |  |

Interpretation: Nitrogen preformed significantly better than Air.

| Ryan-Einot-Gabriel-Welsch Multiple Range Test for Total Defects (Paste x Atmosphere Interaction)  Means with the same REGWQ Grouping letter (A, B) are not significantly different. |        |    |                                |  |  |  |  |
|---|--------|----|--------------------------------|--|--|--|--|
| REGWQ Grouping  | Mean   | N  | Paste x Atmosphere Interaction |  |  |  |  |
| А   | 337.10 | 10 | A Pb-Free with Air             |  |  |  |  |
| В   | 98.70  | 10 | C Pb-Free with Air             |  |  |  |  |
| С   | 15.20  | 10 | B Pb-Free with Air             |  |  |  |  |
| С   | 7.50   | 10 | B Pb-Free with Nitrogen        |  |  |  |  |
| С   | 5.40   | 10 | A Pb-Free with Nitrogen        |  |  |  |  |
| С   | 5.10   | 10 | C Pb-Free with Nitrogen        |  |  |  |  |

**Interpretation:** The A Pb-Free, Air combination was significantly worse than all other combinations. The C Pb-Free, Air combination was significantly worse than all other remaining combinations. The bottom four combinations could not be told statistically apart from each other within the limitations of the current study.

Only in the case of solder Paste B; it was shown that there is no significant difference between the use of Air or Nitrogen. However, as noted earlier this paste exhibited certain process issues relating to the cost of more frequently cleaning the stencil in the production process.

Part of this effort is to develop inspection criteria for Pb-free solder joints. Two items inspected for were shiny appearance and flux residue. Like other effects these may bear on each other. Flux residue is often glossy and may cause a joint to "look better" than a dry joint. This may be further confused with Air versus Nitrogen, as a joint with residue may have less of a tendency to oxidize while cooling than an unprotected surface.

As noted, there is considerable work to be done in terms of mechanical properties (lead pull, ball and chip shear), joint x-rays for voids and BGA flaws, and stress testing via thermal cycling (0 to 100°C) followed by more mechanical testing. Further analysis on lead finishes also is in progress and requires this data.

### **Conclusions to Date**

We have shown the effects of atmosphere, paste selection, and surface finish on visual appearance defects. While Nitrogen and Paste "B" yielded the fewest defects and SMOBC—HASL was significantly worse as a surface finish, the assembly process was not optimized for any of the variable options. Further, throughput and cost can be significant issues that may override some of these results. Other data to be taken needs to be correlated with these findings to further clarify the effects of these variables on solder joint reliability and yield. These data show it is possible to obtain visually acceptable solder joints using a variety of board finishes, lead finishes, paste formulations and Air/Nitrogen combinations. Visual inspection is often the only means of defect detection other than circuit testing, and the two often verify one another thus indicating a good Pb-free reflow process with high yield can be achieved.

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## For more information, please contact us at:

#### Corporate Headquarters

Air Products and Chemicals, Inc. 7201 Hamilton Boulevard Allentown, PA 18195-1501 T 800-654-4567 T 610-706-4730 F 800-272-4449 F 610-706-6890 E gigmrktg@airproducts.com

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